

Reinforcing 3D Printed Polymers with Continuous Stainless Steel Fiber Bundle Allison Goehringer, Alison Clarke and Denis Dowling



Advanced Manufacturing **Research Centre**

Abstract

Recently, fused filament fabrication 3D printing (FFF) has become a more widely applied technology for producing prototyped and end use components. Therefore there is large interest in enhancing the mechanical properties of these parts. One such way of improving these properties is through the use of a composite which effectively polymer adds reinforcement fibers to the filament [1].

The goal of this project is to investigate for the first time the feasibility of 3D printing continuous steel fiber ex-situ in a nylon matrix and evaluate its material characteristics. This involved both the fabrication of steel reinforced nylon filaments along with the printing of parts using these filaments.

Filament Analysis

Extrusion parameters were determined from the material data and experimentally. PLA SSF filament was previously fabricated to understand the extrusion process.

Material	RPM	Fans	H4	H3	H2	H1
Nylon	2.5	78%	231	235	240	225
Nylon Cotton	2.0	26%	238	243	248	243
Nylon SSF	2.0	40%	238	242	245	239

FFF 3D Printing

In addition to extrusion parameters, printing Nylon has more challenges than PLA. Problems include, bed adhesion, warping, under extrusion and inconsistencies in the

Nylon-SSF filament diameter. After printing multiple Nylon calibration Cubes (19), a fiber sandwich was printed (20). This was done to test the polymer matrix impregnation by printing layers of Nylon, placing a layer of steel fiber, and then continuing to print over this layer.



Fig 19. Nylon Calibration Cube

Methodology

Stainless Steel Fiber Natural Arkema Polyamide 11 (Nylon) (SSF)



Methodology

Diameter 14µm

Degradation Temp: 350 °C

A 3Devo Filament Extruder (3Devo) is used to extrude the filament. Pellets, placed in the hopper, were then heated up in four stages through the extruder screw before coming out the nozzle to be cooled and wound onto a spool for printing (4). The temperatures of the heating zones had to be experimentally determined for each material and adjusted for the environment. Slight modifications were made to the set-up in to extrude filament containing continuous steel fibers.

 Table 1. Table of Extrusion Parameters of Nylon

The goal as extrusion progressed was to reduce diameter, thus reducing volume fraction, and evaluate impregnation. Volume fraction was calculated using Equation 1.

Volume Fraction (%) = $100\% \times \frac{V_{SSF}}{V}$ Eq 1.

Nylon with Cotton Fibers	Nylon with SSF
Initial filaments resulted in large di	ameters and low volume fractions.
Fig 7. $2244 \mu m$ $178.8 \mu m$ $200 \mu m$	Fig 10. $2089 \mu m$ $207.7 \mu m$ 245.56μ 200μ
(2.0, 35%, 251, 254, 258, 252) Diameter: 1.96 mm	(2.1, 32%, 233, 241, 245, 236) Diameter: 4.18 mm
VF = 1.1%	VF = 0.025%

Slow Nylon cooling cormed oblong shaped filament, due to the pullers flattening the hot Nylon instead of pulling down to diameter.



(3.5, 35%, 237, 242, 248, 240)

Diameter: 0.47 mm - 1.04 mm

VF = 8.7%

(2.0, 26%, 238, 243, 248, 243)

Diameter: 0.4 mm

VF = 38%



Fig

12.



Fig 20. Fiber Sandwich

Lastly, two layers of Nylon with SSF was printed to observe the cross section of the printed segment (21).



Fig 21. Fused Filament Fabrication of Nylon with SSF

When looked at under a microscope (22), the zoomed in version (23) shows good fiber impregnation and no large air gaps.





Fig 4. The Inside of 3Devo

A pyrometer was used to capture thermal imaging of the system (5) where the hottest part was the nozzle temperature (6). The filament is also quite hot because the SSF acted as a conductor while the cooling fans were aimed at the outside of the filament.







Fig

9.





Conclusion

10 µm

A Stainless Steel Fiber bundle was successfully embedded into the center of the Nylon matrix material to produce a 3D printable filament with a diameter of 0.5 mm and a volume fraction of 1.8%. This material was then printed to show good fiber impregnation.



Fig 5. Continuous Fiber **Experimental Set-Up**

Fig 6. Thermal Imaging of **Continuous Fiber Extrusion**

The quality of the filament was heavily influenced by the temperature. A margin of error of ± 2 degrees Celsius was determined before the extrusion would fail.



Fig 17. Before ILSS Testing

Fig 13. Initial Set-Up Fig 14. Max Deflection Fig 15. After Release

Standard

50

Parameters in form of (RPM, Fans, H4, H3, H2, H1)

conducted according to standard ASTM D2344 [3]. The

Nylon never reached its ultimate stress point and instead

underwent mostly elastic deformation (13-15).

Next, Interlaminar Shear Stress Testing (ILSS) was

Nylon 11 was determined z = 150 to have a shear stress of 5.3 MPa $[\pm 0.5]$ using Equation 2 (16). Force 100

$$F_{abs}(MPa) = 0.75 \times \frac{P_m}{b \times h}$$
 Eq

Microscope analysis of the samples (17-18), show in the red box that the bottom layer failed under tension.



References

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[2] "Nylon 11 / PA 11," Xometry Europe. https://xometry.eu/en/materials/nylon-pa11/

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Standard Travel in mm

Fig 16. Nylon ILSS Samples